

# Modelling and Analysis of Distributed Power-Flow Controller for Induction Motor Drive

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**Abstract**—The growing demand and the aging of networks make it desirable to control the power flow in power transmission systems fast and reliably. The load changes the voltage variation in the transmission lines must be limited, otherwise the consumers equipments are damaged at distributed side. For reducing these types of problems to develop this controller. The DPFC is derived from the unified power-flow controller (UPFC). The DPFC can be considered as a UPFC with an eliminated common dc link. The active power exchange between the shunt and series converters, which is through the common dc link in the UPFC, is now through the transmission lines at the third-harmonic frequency. The DPFC employs the distributed FACTS (D-FACTS) concept, which is to use multiple small-size single-phase converters instead of the one large-size three-phase series converter in the UPFC.

The large number of series converters provides redundancy, thereby increasing the system reliability. As the D-FACTS converters are single-phase and floating with respect to the ground, there is no high-voltage isolation required between the phases. Accordingly, the cost of the DPFC system is lower than the UPFC. The DPFC has the same control capability as the UPFC, which comprises the adjustment of the line impedance, the transmission angle, and the bus voltage. This paper consists of both active and reactive variations, using MATLAB/SIMULINK is simulated and its effects on the transmission lines observed. DPFC for induction motor drive applications are also proposed. The different applications of induction motor simulated using MATLAB/SIMULINK software.

**Index Terms**— Induction motor, AC-DC power conversion, load flow control, power electronics, power semiconductor devices, power system control, power-transmission control.

## 1. INTRODUCTION

This paper discusses the concept of a distributed approach for realizing FACTS devices, in particular series FACTS devices. The increasing performance and decreasing price of electronics, power electronics and communications technologies have transformed entire industry sectors. It is proposed that a similar approach to the implementation of high power FACTS devices can provide a higher performance and lower cost method for enhancing T&D system reliability and controllability, improving asset utilization and end-user power quality, while minimizing system cost and environmental impact. The main purpose of this technology is to control and regulate the electric power in transmission systems.

This is achieved by using converters as a controllable interface between two power system terminals. The resulting converter representations can be useful for a variety of configurations. The static compensator (STATCOM) is a shunt connected device that is able to provide reactive power support at a network location far away from the generators. Through this reactive power injection, the STATCOM can regulate the voltage at the connection node. The static synchronous series compensator (SSSC) is a series device which injects a voltage in series with the transmission line. Ideally, this injected voltage is in quadrature with the line current, such that the SSSC behaves like an inductor or a capacitor for the purpose of increasing or decreasing the overall reactive voltage drop across the line, and thereby, controlling the transmitted power. In this operating mode, the SSSC does not interchange any real power with the system in steady-state.

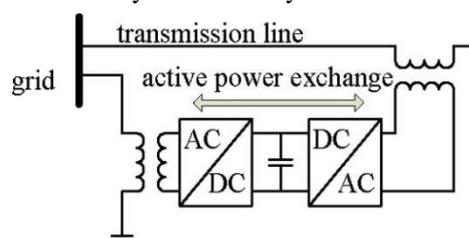


Fig 1: Simplified representation of a UPFC

The unified power-flow controller (UPFC) is the most versatile device of the family of FACTS devices, since it is able to control the active and the reactive power, respectively, as well as the voltage at the connection node. The unified power-flow controller (UPFC) is comprised of a STATCOM and a SSSC, coupled via a common DC link to allow bi-directional flow of active power between the series output terminals of the SSSC and the shunt output terminals of the STATCOM. Each converter can independently generate (or) absorb reactive power at its own AC terminal. The two converters are operated from a DC link provided by a DC storage capacitor.

The UPFC is not widely applied in practice, due to their high cost and the susceptibility to failures. Generally, the reliability can be improved by reducing the number of components; however, this is not possible due to the complex topology of the UPFC. To reduce the failure rate of the components, selecting components with higher ratings than necessary or employing redundancy at the component or system levels. Unfortunately, these solutions increase the initial investment necessary, negating any cost related advantages. Accordingly, new approaches are needed in order to increase reliability and reduce cost of the UPFC.

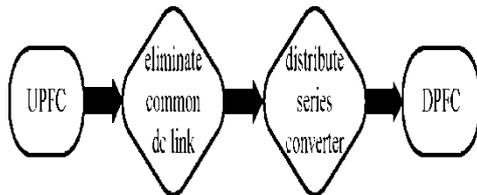


Fig 2: Flowchart from UPFC to DPFC

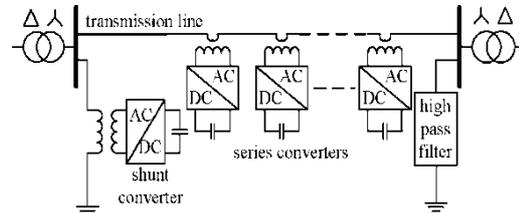
The same as the UPFC, the DPFC is able to control all system parameters like line impedance, transmission angle & bus voltage. The DPFC eliminates the common dc link between the shunt and series converters. The series converter of the DPFC employs the distributed FACTS (D-FACTS) concept. Comparing with the UPFC, the DPFC have two major advantages: 1) low cost because of the low voltage isolation and the low component rating of the series converter and 2) High reliability because of the redundancy of the series converters and high control capability. DPFC can also be used to improve the power quality and system stability such as power oscillation damping, voltage sag restoration or balancing asymmetry.

**II. DPFC Topology**

By introducing the two approaches outlined in the previous section (elimination of the common DC link and distribution of the series converter) into the UPFC, the DPFC is achieved. Similar as the UPFC, the DPFC consists of shunt and series connected converters. The shunt converter is similar as a STATCOM, while the series converter

employs the DSSC concept, which is to use multiple single -phase converters instead of one three-phase converter. Each converter within the DPFC is independent and has its own DC capacitor to provide the required DC voltage. The configuration of the DPFC is shown in Figure 3.

Fig 3: DPFC configuration



As shown, besides the key components - shunt and series converters, a DPFC also requires a high pass filter that is shunt connected to the other side of the transmission line and a Y-Δ transformer on each side of the line. The reason for these extra components will be explained later. The unique control capability of the UPFC is given by the back-to-back connection between the shunt and series converters, which allows the active power to freely exchange. To ensure the DPFC has the same control capability as the UPFC, a method that allows active power exchange between converters with an eliminated DC link is required.

**III. DPFC Operating Principle**

**1. Active power exchange with eliminated DC link**

According to the Fourier analysis, non-sinusoidal voltage and current can be expressed as the sum of sinusoidal functions in different frequencies with different amplitudes. The active power resulting from this non-sinusoidal voltage and current is defined as the mean value of the product of voltage and current. Since the integrals of all the cross product of terms with different frequencies are zero, the active power can be expressed by:

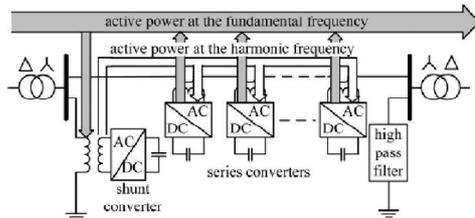
$$P = \sum_{i=1}^{\infty} V_i I_i \cos \phi_i \quad \text{--- (1)}$$

Where  $V_i$  and  $I_i$  are the voltage and current at the  $i_{th}$  harmonic frequency respectively, and  $\phi_i$  is the corresponding angle between the voltage and current. Equation (1) shown that the active powers at different frequencies are independent from each other and the voltage or current at one frequency has no influence on the active power at other frequencies.

By applying this method to the DPFC, the shunt converter can absorb active power from the grid at the fundamental frequency and inject the power back at a harmonic frequency. This harmonic active power flows through a transmission line equipped with series converters. According to the amount of required active power

at the fundamental frequency, the DPFC series converters generate a voltage at the harmonic frequency, thereby absorbing the active power from harmonic components.

Neglecting losses, the active power generated at the fundamental frequency is equal to the power absorbed at the harmonic frequency. Fig.4 indicates how the active power is exchanged between the shunt and series converters in the DPFC system.

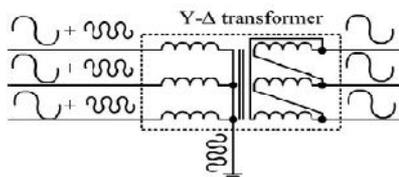


**Fig 4: Active power exchange between DPFC converters**

The high-pass filter within the DPFC blocks the fundamental frequency components and allows the harmonic components to pass, thereby providing a return path for the harmonic components. The shunt and series converters, the high pass filter and the ground from a closed loop for the harmonic current.

**2. Using third harmonic components**

Due to the unique features of 3rd harmonic frequency components in a three-phase system, the 3rd harmonic is selected for active power exchange in the DPFC. In a three-phase system, the 3rd harmonic in each phase is identical, which means they are ‘zero -sequence’ components. Because the zero-sequence harmonic can be naturally blocked by Y-Δ transformers and these are widely incorporated in power systems (as a means of changing voltage), there is no extra filter required to prevent harmonic leakage. As introduced above, a high-pass filter is required to make a closed loop for the harmonic current and the cut off frequency of this filter is approximately the fundamental frequency.

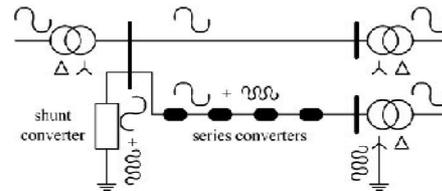


**Fig 5: Utilize grounded Y-Δ transformer to filter zero- sequence harmonic**

Because the voltage isolation is high and the harmonic frequency is close to the cut off frequency, the filter will be costly. By using the zero-sequence harmonic, the costly filter can be replaced by a cable that connects the neutral point of the Y-Δ transformer on the right side in Fig 4.with the ground. Because the Δ-winding appears open-circuit to the 3rd harmonic current, all

harmonic current will flow through the Y-winding and concentrate to the grounding cable as shown in Fig 5. Therefore, the large high-pass filter is eliminated.

Another advantage of using the 3rd harmonic to exchange active power is that the grounding of the Y-Δ transformers can be used to route the harmonic current in a meshed network. If the network requires the harmonic current to flow through a specific branch, the neutral point of the Y-Δ transformer in that branch, at the side opposite to the shunt converter, will be grounded and vice versa.



**Fig 6: Route the harmonic current by using the grounding of the Y-Δ transformer**

Fig 6 shows a simple example of routing the harmonic current by using the grounding Y-Δ of the transformer. Because the floating neutral point is located on the transformer of the line without the series converter, it is an open-circuit for 3rd harmonic components and therefore no 3rd harmonic current will flow through this line.

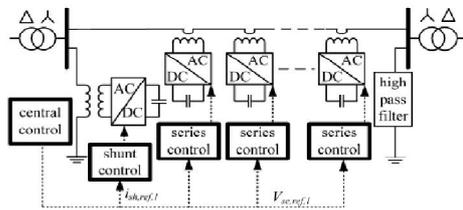
The harmonic at the frequencies like 3rd, 6th, 9th... are all zero-sequence and all can be used to exchange active power in the DPFC. However, the 3rd harmonic is selected, because it is the lowest frequency among all zero-sequence harmonics. The relationship between the exchanged active power at the  $i^{th}$  harmonic frequency  $P_i$  and the voltages generated by the converters is expressed by the well known the power flow equation and given as:

$$P_i = \frac{|V_{sh,i}| |V_{se,i}|}{X_i} \sin(\theta_{sh,i} - \theta_{se,i}) \quad \text{--- (2)}$$

Where  $X_i$  is the line impedance at  $i^{th}$  frequency,  $|V_{sh,i}|$  and  $|V_{se,i}|$  and is the voltage magnitudes of the  $i^{th}$  harmonic of the shunt and series converters, and  $\theta_{sh,i} - \theta_{se,i}$  is the angle difference between the two voltages. As shown, the impedance of the line limits the active power exchange capacity. To exchange the same amount of active power, the line with high impedance requires higher voltages. Because the transmission line impedance is mostly inductive and proportional to frequency, high transmission frequencies will cause high impedance and result in high voltage within converters. Consequently, the zero - sequence harmonic with the lowest frequency - the 3rd harmonic - has been selected.

**IV. DPFC Control**

To control multiple converters, a DPFC consists of three types of controllers: central control, shunt control and series control, as shown in Fig 7.



**Fig 7: DPFC control block diagram**

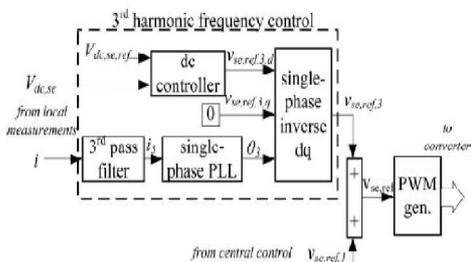
The shunt and series control are localized controllers and are responsible for maintaining their own converters' parameters. The central control takes care of the DPFC functions at the power system level. The function of each controller is listed:

**1) Central control:**

The central control generates the reference signals for both the shunt and series converters of the DPFC. Its control function depends on the specifics of the DPFC applicant ion at the power system level, such as power flow control, low frequency power oscillation damping and balancing of asymmetrical components. According to the system requirements, the central control gives corresponding voltage reference signals for the series converters and reactive current signal for the shunt converter. All the reference signals generated by the central control concern the fundamental frequency components.

**2) Series control:**

Each series converter has its own series control. The controller is used to maintain the capacitor DC voltage of its own converter, by using 3<sup>rd</sup> harmonic frequency components, in addition to generating series voltage at the fundamental frequency as required by the central control.



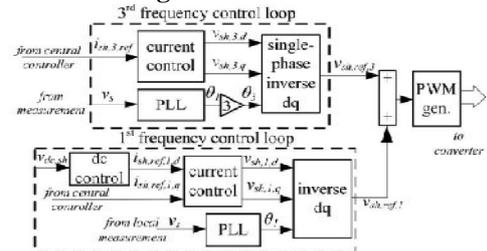
**Fig 8: Block diagram of the series converter control**

**3) Shunt control:**

The objective of the shunt control is to inject a constant 3<sup>rd</sup> harmonic current into the line to supply active power for the series converters. At the same time, it maintains the capacitor DC voltage of the shunt converter at a constant value by absorbing active power from the grid at the

fundamental frequency and injecting the required reactive current at the fundamental frequency into the grid to keep the capacitor dc voltage at a constant level.

**Fig 9: Block diagram of the shunt converter**



**control**

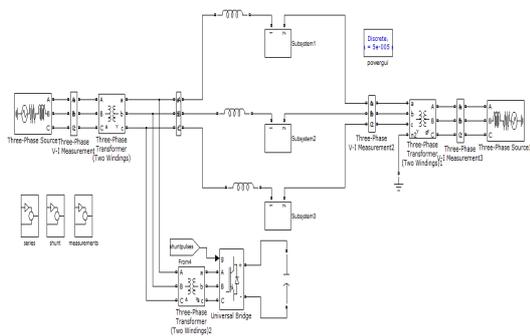
The control for the fundamental frequency components consists of two cascaded controllers. The current control is the inner control loop, which is to modulate the shunt current at the fundamental frequency. The q-component of the reference signal of the shunt converter is obtained from the central controller and d- component is generated by the dc control.

**V. MATLAB/SIMULATION RESULTS**

**Case: 1 Implementation of Proposed DPFC**

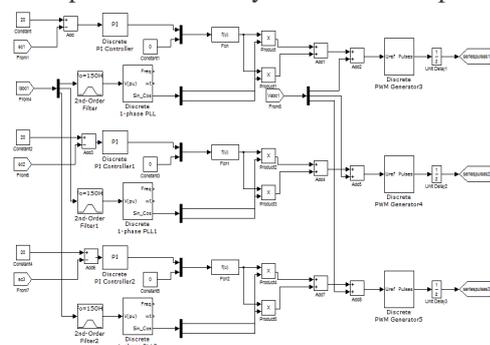
One shunt converter and three single-phase series converters are built and tested in a scaled network, as shown in Fig 10.

**Fig 10: Simulated Model for DPFC**



**5.1) Series converter SIMULINK Model**

Within the setup, multiple series converters are controlled by a central controller. The central controller gives the reference voltage signals for all series converters. The voltages and current within the setup are measured by its simulink outputs.



**Fig 11: Simulated model for series converter**

**5.2) Shunt converter SIMULINK Model**

The basic function of the shunt converter is to supply or absorb the active power demand by the series converter. The shunt converter controls the voltage of the DC capacitor by absorbing or generating active power from the bus, therefore it acts as a synchronous source in parallel with the system. To verify the DPFC principle, two situations are demonstrated: the DPFC behaviour in steady state and the step response. In steady state, the series converter is controlled to insert a voltage vector with both d and q component, which is  $V_{se,d,ref} = 0.3V$  and  $V_{se,q,ref} = -0.1V$ . Figs.13-17 show one operation point of the DPFC setup. The voltage injected by the series converter, the current through the line, and the voltage and current at the  $\Delta$  side of the transformer.

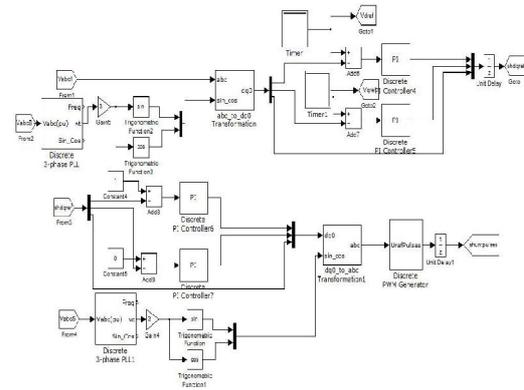


Fig 12: Simulated model for shunt converter

The DPFC controls the power flow through transmission lines by varying the voltage injected by the series converter at the fundamental frequency. Figs. 13-17 illustrate the step response of the experimental setup. A step change of the fundamental reference voltage of the series converter is made, which consists of both active and reactive variations, as shown in Fig. 13.

As shown, the dc voltage of the series converter is stabilized before and after the step change. To verify if the series converter can inject or absorb active and reactive power from the grid at the fundamental frequency, the power is calculated from the measured voltage and current in Figs. 14 and 15. The measured data in one phase are processed in the computer by using MATLAB. To analyze the voltage and current at the fundamental frequency, the measured data that contains harmonic distortion are filtered by a low-pass digital filter with the 50-Hz cut off frequency. Because of this filter, the calculated voltage and current at the fundamental frequency have a 1.5 cycle delay to the actual values, thereby causing a delay of the measured active and reactive power. Fig. 16 illustrated the active and reactive power injected by the series converter. A comparison is made between the measured power and the calculated power. We can see that the series converters are able to absorb and inject both active

and reactive power to the grid at the fundamental frequency.

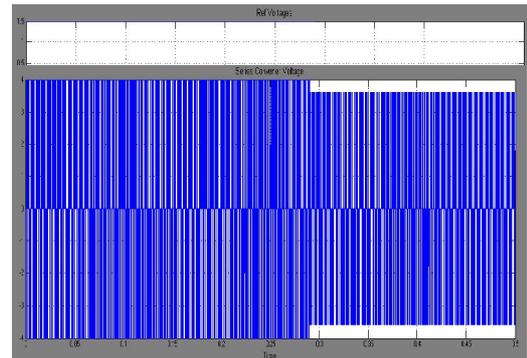
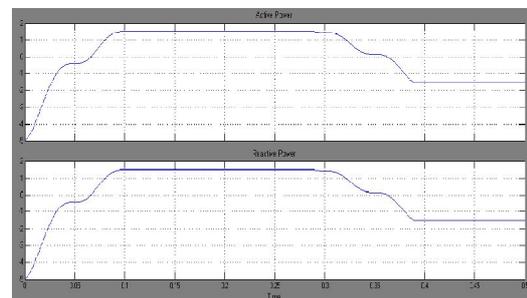
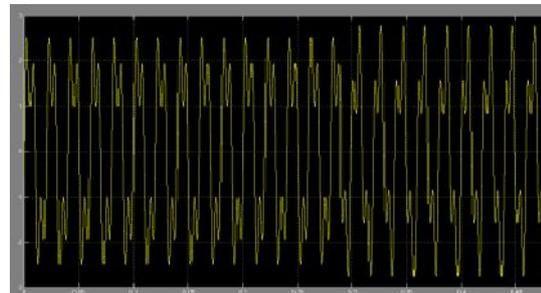


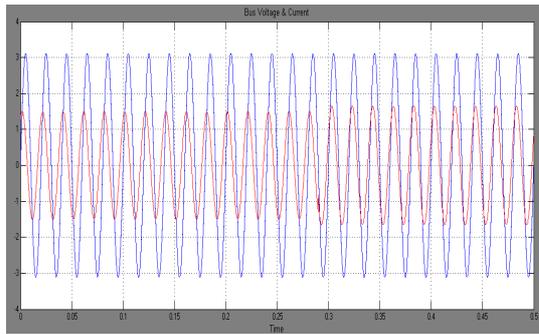
Fig 13: Reference voltage for the series converters

Fig 14: Step response of the DPFC: series converter voltage

Fig 15: Step response of the DPFC: line current

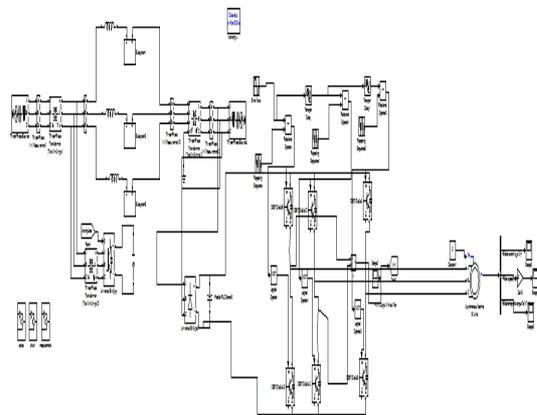
Fig 16: Step response of the DPFC: active and reactive power injected by the series converter at the fundamental frequency



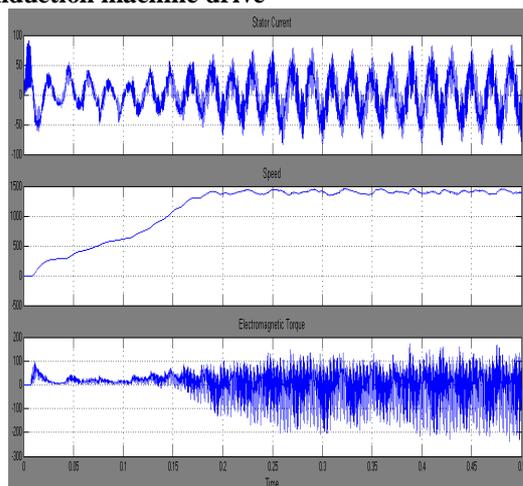


**Fig 17: Step response of the DPFC: bus voltage and current at the  $\Delta$  side of the transformer.**

### Case: 2 Implementation of Proposed DPFC with Induction Machine Drive



**Fig 18: Simulated model of the DPFC with induction machine drive**



**Fig 19: Stator Current, Speed, Electromagnetic Torque**

## VI. CONCLUSION

This paper has presented a new concept called DPFC. The DPFC emerges from the UPFC. It inherits the control capability of the UPFC, which

is the simultaneous adjustment of the line impedance, the transmission angle, and the bus-voltage magnitude. The common dc link between the shunt and series converters, which is used for exchanging active power in the UPFC, is eliminated. This power is now transmitted through the transmission line at the third-harmonic frequency. The series converter of the DPFC employs the D-FACTS concept, which uses multiple small single-phase converters instead of one large-size converter. The reliability of the DPFC is greatly increased because of the redundancy of the series converters. The total cost of the DPFC is also much lower than the UPFC, because no high-voltage isolation is required at the series-converter part and the rating of the components is low. The DPFC concept has been verified by an experimental setup. It is proved that the shunt and series converters in the DPFC can exchange active power at the third-harmonic frequency, and the series converters are able to inject controllable active and reactive power at the fundamental frequency.

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